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STATEMENT OF VERIFIED ENGLISH TRANSLATION

Assistant Commissioner
For Patents
Washington, D.C. 20231

Dear Sir:

The undersigned translator is fluent in German and English and that to the best of his/her knowledge and belief, the enclosed is a true and accurate translation of the German-language PCT Patent Application No. PCT/EP03/05402

The undersigned further declares that all statements made herein of his/her own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code and that such willful and false statements may jeopardize the validity of the application or any patent issuing thereon.

By: Sabine Schmidt Date: October 1, 2004

(Typed Name of Translator)

Sabine Schmidt

(Signature of Translator)

Am Hirschsprung 46
51109 Köln, Germany

(Address of Translator)

Replaced by translation
TITLE OF THE INVENTION *Dated 16 Jun 05*

Two-shaft vacuum pump

BACKGROUND OF THE INVENTION

Field of the invention

The invention relates to a two-shaft vacuum pump comprising two shafts.

5 Description of related art

The rolling piston pump, also referred to as Roots pump, is a typical two-shaft vacuum pump. Both shafts of the Roots pump comprise a rolling piston which roll off without contacting each other. One of the two shafts is driven by an 10 electric drive motor, while the other shaft is synchronized with the drive shaft by means of a gear. During pumping operation the rolling pistons are strongly heated due to the gas compression.

In practice, only asynchronous motors are used as drive motors. The motor 15 rotor of the asynchronous motor arranged on the drive shaft is configured as a so-called cage rotor. The motor rotor configured as a cage rotor has a relatively large mass and axial overall length. Due to the necessarily resulting large unbalance forces and the vibrations resulting from the latter, the drive shaft must be supported by at least one supporting bearing in the area of the 20 drive motor. Cooling and lubrication of the supporting bearing or bearings are, in particular owing to its/their arrangement in the gas-tightly sealed area of the vacuum pump, problematic and can be realized only at a high effort and expenditure.

25 From DE-A-38 28 608, which represents the prior art as referred to in the precharacterizing part of claim 1, a vacuum rolling piston pump is known which is driven by a synchronous motor. The concrete configuration of the

motor rotor is not described. Synchronous motors are generally not suitable for use in vacuum pumps because the motor rotor is separately excited via heat-producing sliding contacts. A permanently excited synchronous motor rotor is unsuitable because it supplies, due to the constant rotor excitation, a 5 torque maintained constant via the speed, and overheating of the pump rotor may occur at higher speeds. In the practice, synchronous motors are therefore not used for driving vacuum pumps.

SUMMARY OF THE INVENTION

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It is an object of the invention to provide a two-shaft vacuum pump with an improved drive.

15 1.

According to the invention, the drive motor is a synchronous motor, wherein the rotor is configured such that it is permanently excited by a permanent magnet. The permanently excited rotor of a synchronous motor has a small 20 mass and a small overall length due to the constantly strong magnetic field and the low power loss. Owing to this fact, all shaft supporting bearings for additionally supporting the drive shaft may possibly be omitted, whereby the problems associated with cooling and lubrication of the supporting bearings are eliminated either.

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Due to the lower power loss in the permanently excited rotor, heating-up of the rotor and the problems associated with said heating-up are reduced, too.

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Further, a synchronous motor power-limiting means is provided which limits the motor power to a fixed maximum motor power in a limiting range above a fixed rated motor speed. The power-limiting means limits the driving power to

a constant value at a speed above the rated speed. This is effected by reduction of the torque at a shaft speed above the rated speed.

The motor power results from the following equation:

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$$P_M = M_M \times \omega,$$

where

10 $\omega = 2\pi \cdot n,$

P_M is the motor power,

M_M is the motor speed at speed n , and

n is the motor speed.

15 The speed reduction in the limiting range ensures that the pump is capable of operating at high speeds of up to 8,000 revolutions per minute, but the pumping capacity is limited to a constant maximum value. The possibilities of dissipating the rolling piston heat are strongly restricted by the low gas pressure and the configuration. By limiting the motor power and thus the pumping

20 capacity without simultaneous speed limitation, overheating of the vacuum pump and in particular the rolling pistons is reliably prevented, wherein, at the same time, a high gas volume flow is maintained. In the limiting range, the synchronous motor is operated in the so-called field-weakening range.

25 The magnetic flux of the permanently magnetized motor rotor is constant such that a change in the motor torque can be effected only by a corresponding control of the stator field.

30 In practical applications, permanently excited motor rotors have so far not been used in vacuum pumps because due to the torque, which is maintained constant over the overall speed range owing to the operating principle applied, there was the danger of overheating of the rotor at high speeds caused

by the compression heat which increases with the speed. In view of these drawbacks it has so far seemed unrealistic or impossible to use a permanently excited synchronous motor for driving a vacuum pump. Owing to the limitation of the motor power in the limiting range caused by the field-weakening 5 operation the compression-induced heating of the motor rotor is limited to a constant value at higher speeds. Only this makes the use of a permanently excited synchronous motor possible and sensible, wherein the maximum torque of the motor can be made use of until the limiting range has been reached.

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According to a preferred aspect, the power-limiting means adjusts, in the limiting range, the phase angle between the electrical stator field and the magnetic field of the motor to an angle other than 90 degrees. The phase position of the electrical stator field is adjusted relative to the magnetic field of the 15 rotor such that the torque is correspondingly reduced.

Alternatively or supplementary, the power-limiting means reduces, in the limiting range, the amount of the stator current. This, too, reduces the torque M_M which is proportional to the stator current.

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According to a preferred aspect, the power-limiting means adjusts, in the limiting range, the phase angle and/or the stator current as a function of the speed. With increasing speed in the limiting range between the rated speed and the maximum speed, the phase angle and/or the stator current are 25 changed such that the torque decreases with increasing speed to such an extent that the motor power above the rated speed is always nearly constant. Thus, the maximum permissible motor power is made available, but not exceeded, at each speed. The vacuum pump is protected against overheating.

30 According to a preferred aspect, the shaft comprising the motor rotor is of overhung configuration and supported without a supporting bearing at the motor-side end. The shaft is exclusively supported by the two main bearings

arranged at the two longitudinal ends of the pump rotor. The structures required for cooling and lubricating motor supporting bearings are omitted.

5 Preferably, the motor rotor comprises a plurality of permanent magnets arranged on the outside of the motor rotor body. It is also possible that one or a plurality of permanent magnets are arranged in a corresponding recess of the motor rotor body.

10 Preferably, the motor rotor comprises, in particular for operation with gases which may damage the motor materials, a rotor enclosure of a nonmagnetic material, which externally encloses the motor rotor body and the permanent magnets. Thus the permanent magnets disposed on the outside of the motor rotor body are secured and protected against any aggressive gases and liquids and thus against corrosion. The rotor enclosure may be made from a 15 nonmagnetic metall or a plastic material.

20 According to a preferred aspect, a can of a nonmagnetic material is provided on the stator side, which can gas-tightly seals the rotor towards the stator. The can is made from a nonmagnetic material or a plastic material. The can gas-tightly seals the pump area towards the surroundings, wherein the motor rotor lies within the pump area and the motor stator lies outside the pump area. Due to the use of a permanently excited synchronous motor the gap between rotor and stator may be relatively large. This facilitates the insertion of a can.

25 According to a preferred aspect, a pump cover holding the can and a stator casing surrounding the motor stator are integrally formed. This configuration reduces the number of components and the number of joints.

30 Preferably, the permanent magnet is made from rare earths. With permanent magnets of rare earths strong magnetic fields of long duration can be realized at a small overall length.

BRIEF DESCRIPTION OF THE DRAWINGS

Hereunder an embodiment of the invention is explained in detail with reference to the drawings in which:

Fig. 1 shows a longitudinal section of a two-shaft vacuum pump,

Fig. 2 shows a detail of the drive motor of the vacuum pump shown in Fig. 1, and

Fig. 3 shows schematic representation showing the motor power, the motor torque, the pump moment characteristic curve and the pumping capacity of the vacuum pump shown in Figs. 1 and 2 obtained with a 4.8 kW drive motor.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENT OF THE INVENTION

Fig. 1 shows a two-shaft vacuum pump 10 configured as a rolling-piston pump comprising two rotor shafts 12,14. Each rotor shaft 12,14 comprises a pump rotor 16,18 configured as a rolling piston. One of the rotor shafts 14 is driven by an electric drive motor 20, while the other shaft 12 is driven by a gear 24 formed by two toothed wheels 22,23 and synchronized with one rotor shaft 14.

The drive motor 20 is a synchronous motor and essentially comprises a permanently excited motor rotor 26 and a motor stator 28 having a plurality of stator coils 30,31.

The configuration of the motor rotor 26 is shown in an enlarged representation in Fig. 2: the motor rotor 26 comprises a pot-shaped rotor body 34 pro-

vided on its outer circumference with a plurality of recesses 36 into each of which a permanent magnet 38 of rare earths is glued. The overall outer circumference of the rotor 26 is enclosed by a cylindrical rotor enclosure 40 of a nonmagnetic material. The rotor enclosure 40 retains the permanent magnets 38 in the recesses 36 even at high rotor speeds and reliably shields the permanent magnets 38 against corrosion-developing gases and liquids. The rotor enclosure 40 is made from nonmagnetic high-grade steel, it may however also be made from a carbon fiber-reinforced plastic material or other nonmagnetic materials. The rotor body 34 can be of laminated or solid configuration. Between the rotor 26 and the stator 28 a pot-shaped can 42 is provided which is attached to a motor casing 44 on the stator side. The can gas-tightly seals the motor rotor 26 towards the stator 28. The can 42 is made from nonmagnetic high-grade steel, but can also be made from carbon fiber-reinforced plastic material or other nonmagnetic materials.

15 Due to its configuration as a synchronous motor rotor permanently excited by permanent magnets 38, the motor rotor 26 has a small axial overall length and a small mass. This allows the shaft 14 carrying the motor rotor 26 to be supported by two pump rotor rolling bearings 46,47 alone and its motor-side 20 end to be configured without a supporting bearing. The motor rotor 26 is thus of completely overhung configuration.

The motor casing 44 is configured in one piece and comprises a pump cover 48 holding the can 42 and a stator casing 50 surrounding the motor stator 28. 25 The pump cover 48 holds the can 42 and gas-tightly seals the suction chamber 52 towards the outside. In a housing 54 placed on the outside of the motor casing 44 a motor control 56 is accommodated. The motor control 56 controls the supply of the stator coils 30,31.

30 The motor control 56 comprises a synchronous motor power-limiting means 58 which, above a fixed rated motor speed n_N , limits the motor power P_M to a fixed maximum motor power $P_{M\max}$, as shown in Fig. 3. Thus, the maximum

pumping capacity is limited to a maximum value. This is necessary to prevent overheating of the pump rotors 16,18. The motor control 56 further comprises a frequency converter for starting up the drive motor and controlling the speed.

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The motor power P_M results from the following equation:

$$P_M = \omega \cdot M_M,$$

where $\omega = 2\pi \cdot n$, n is the speed, and M_M is the motor torque. At increasing

10 speed the motor power limitation can thus be effected only by reducing the motor torque M_M .

The speed range between the rated speed n_N , at which the maximum motor power $P_{M\max}$ is reached, and the maximum speed n_{\max} is referred to as limiting

15 range. Since the magnetic flux generated by the permanently excited motor rotor 26 is always constant, the torque in the limiting range can be obtained only by correspondingly controlling the stator coils 30,31. In the limiting range the stator coils 30,31 are thus controlled such that the torque is reduced with increasing speed and reciprocally proportional to the speed. In the 20 limiting range the drive motor 20 is operated in the so-called field-weakening range.

For this purpose, in the limiting range the stator current is reduced in accordance with the necessary torque reduction. Alternatively or supplementary,

25 the power-limiting means 58 can adjust, in the limiting range, the phase angle between the magnetic field of the motor and the electrical stator field to an angle other than 90°. The control of the motor current and/or the phase angle in the limiting range is always effected as a function of the speed.

30 Fig. 3 shows that the pump torque M_P and the pumping capacity P_P are always somewhat below the motor torque M_M and the motor power P_M , respectively,

due to friction losses etc. Overheating of the pump rotor is excluded when the maximum pumping capacity and motor power are correctly calculated and adjusted.

- 5 Although the invention has been described and illustrated with reference to specific illustrative embodiments thereof, it is not intended that the invention be limited to those illustrative embodiments. Those skilled in the art will recognize that variations and modifications can be made without departing from the true scope of the invention as defined by the claims that follow. It is
- 10 therefore intended to include within the invention all such variations and modifications as fall within the scope of the appended claims and equivalents thereof.